

such membranes be easily manufactured at low cost without the use of hazardous substances. Furthermore, ideal membranes should be easy to handle and process and should also be amenable to low cost assembly techniques during the production of devices containing such membranes.

Current commercially available ion exchange membranes are primarily of two general types:

5 homogeneous membranes and heterogeneous membranes. A homogeneous membrane is one in which the entire volume of the membrane (excluding any support material that may be used to improve strength) is made from the reactive polymer. Examples include membranes made of sulfonated or aminated styrene-divinylbenzene polymers (SDVB membranes), polymerized perfluorosulfonic acids (PFSO membranes) or various thermoplastics with active groups grafted onto
10 the base polymer.

Unfortunately, homogeneous membranes tend to be difficult to manufacture. They also tend to employ the use of hazardous materials during their manufacturing process since, for the most part, they must be made from base monomers. Additionally, they are difficult to modify chemically because each modification requires a change in the fundamental chemistry of the membrane.

15 Homogeneous membranes also tend to have limited physical strength (therefore often requiring a screen or cloth support) because the polymer produced cannot readily combine both the required physical and electrochemical properties to operate efficiently in a fabricated device. Homogeneous membranes may be either crosslinked (to provide the membrane with dimensional stability, but increased brittleness and sensitivity upon drying), or they may be non-crosslinked (to
20 provide membranes which may be dried, but lack dimensional stability and resistance to swelling and various solvents).

In contrast, heterogeneous membranes are formed of 1) a composite containing an ion exchange resin to impart electrochemical properties and 2) a binder to impart physical strength and integrity. Typical heterogeneous membranes may be produced as "micro-heterogeneous" membranes by the paste method (in which ion exchange resin monomers are reacted to form the ultimate ion exchange resin polymer in the presence of a finely-ground inert binder polymer), or in the alternative, as "macro-heterogeneous" membranes by the physical blending of pre-polymerized ion exchange resin and binder.

Present macro-heterogeneous membranes tend to have inferior electrochemical properties as compared to micro-heterogeneous membranes, but they do offer a number of advantages as compared to membranes of the micro-heterogeneous variety. In particular, macro-heterogeneous membranes are easy to manufacture and can be readily chemically modified since, within limits, the binder and resin types and content can be varied without significantly modifying the manufacturing process. Notably, with micro-heterogeneous membranes, the binder must be compatible with the pre-cursor ion exchange monomers such that the binder does not interfere with the polymerization of the ion exchange monomer or, as a consequence of such polymerization, becomes chemically altered with undesirable properties.

In some filter-press type unit operations, ion exchange membranes are typically interposed between adjacent frame members to assist in defining individual chambers or compartments. For example, in filter-press type electrodeionization units, ion exchange membranes are interposed between adjacent frame members or spacers to form separate diluting and concentrating chambers. In assembling such units, a plurality of frame members are provided in a parallel manner with ion

exchange membranes interposed between the frame members. The resulting structure is then forced together by clamping means with a view to providing a closed, tightly sealed unit.

Unfortunately, present ion exchange membrane materials do not possess entirely adequate sealing characteristics. During prolonged operation of the afore-mentioned unit operations, ion exchange membrane materials have a tendency to creep, thereby receding from contact with adjacent frame members and potentially compromising positive sealing of the unit. Present ion exchange membranes also tend to be brittle and prone to tearing or pinhole formation, thereby further potentially compromising the sealing of the unit.

In addition, present ion exchange materials are not particularly suitable for high temperature applications. As a result, unit operations having ion exchange membranes are unlikely candidates for pharmaceutical applications, where the constituent membranes would be exposed to high temperatures during cleaning for purposes of disinfection.

With respect to membrane manufacturing, the prior methods used to make heterogeneous ion exchange membranes involved standard equipment for sheet extrusion. This equipment is very common. However, extruding filled materials like heterogeneous ion exchange membranes involves special difficulties. Gauge control, gear pump pressure limits and uniformity of dispersion of the phases are all special difficulties encountered when extruding the materials in question. Yield rates as low as 30% are common.

Summary of Invention

A heterogeneous ion exchange material is provided comprising an ion exchange resin incorporated within a binder, the binder comprising a material selected from the group consisting

of (i) a polyolefin, copolymerized by single site catalyst technology, (ii) a very low density polyethylene or ultra low density polyethylene processed using either Ziegler-Natta catalysts or Metallocene catalysts, (iii) a thermoplastic elastomeric olefin comprising a polypropylene continuous phase with an ethylene-propylene-diene monomer or ethylene-propylene rubber rubbery phase dispersed through the polypropylene continuous phase, and (iv) a thermoplastic vulcanizate comprising a polypropylene continuous phase with an ethylene-propylene-diene monomer, ethylene-propylene rubber, nitrile-butadiene rubber, natural rubber, ethylene vinyl acetate rubbery phase dispersed through the polypropylene continuous phase, a co-polymer of vinylidene fluoride and hexafluoropropylene, or a co-polymer of vinylidene fluoride and hexafluoropropylene and tetrafluoroethylene.

In one aspect, the binder is a Metallocene catalyzed polyolefin..

In another aspect, the binder is a very low density polyethylene or ultra low density polyethylene processed using either Ziegler-Natta catalysts or Metallocene catalysts.

In a further aspect, the binder is a thermoplastic elastomeric olefin comprising a polypropylene continuous phase with an ethylene-propylene-diene monomer or ethylene-propylene rubber rubbery phase dispersed through the polypropylene continuous phase.

In yet a further aspect, the binder is a thermoplastic vulcanizate comprising a polypropylene continuous phase with an ethylene-propylene-diene monomer, ethylene-propylene rubber, nitrile-butadiene rubber, natural rubber or ethylene vinyl acetate rubbery phase dispersed through the polypropylene continuous phase.

A method for manufacturing an ion exchange membrane is also provided using advanced extrusion techniques, including computer-controlled material feed, computer-controlled automatic

A method for manufacturing an ion exchange membrane is also provided by injection molding.

Brief Description of Drawings

The present invention will be better understood with reference to the appended drawings in which:

Figure 1 is an illustration of an auto-die;

Figure 2 is a schematic of a method of manufacturing an ion exchange membrane.

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In one embodiment, the polyolefin is an alpha-olefin co-polymer, characterized by a crystallinity of less than 40%.. Suitable alpha-olefin co-monomers include C₄ - C₁₂ alpha-olefins.

In one embodiment, the alpha-olefin co-monomer is octene.

5 In another embodiment, the polyolefin is an ethylene alpha-olefin copolymer, copolymerized using single-site catalyst technology, such as a metallocene catalyst. An example of such suitable ethylene alpha-olefins are ENGAGE™ polyolefin elastomers manufactured by DuPont Dow Elastomers.

10 In one embodiment, the ethylene alpha-olefin copolymer, copolymerized using single-site catalyst technology, is ethylene-octene copolymer. Octene content ranges from 16 to 40 wt%, Mooney viscosity is from 1.5 to 35, measured according to ASTM D1646ML. Density is within the range of from 0.860 to 0.920 g/cm³. In another embodiment, the density is from 0.885 to 0.913 g/cm³. The melt index is from 0.5 to 30 dg/min, measured according to ASTM D-1238.

15 In one embodiment, the thermoplastic based elastomer is an alloy comprising a metallocene catalyzed polyolefin and any of polypropylene (PP), low density polyethylene (LDPE), high density polyethylene (HDPE), EDPM (cross-linked, partially cross-linked, or non-cross-linked), EPR (cross-linked, partially cross-linked, or non-cross-linked), EVA, or other synthetic rubbers such as a co-polymer of vinylidene fluoride and hexafluoropropylene, or a co-polymer of vinylidene fluoride and hexafluoropropylene and tetrafluoroethylene.

20 In another embodiment, the thermoplastic based elastomer is an alloy of VLDPE or ULDPE and any of PP, LDPE, HDPE, metallocene catalyzed polyolefin, EPDM, (cross-linked, partially cross-linked, or non-cross-linked), EPR (cross-linked, partially cross-linked, or non-cross-linked) or EVA.

In another embodiment, the thermoplastic based elastomer is an alloy of (i) a thermoplastic elastomeric olefin comprising a polypropylene continuous phase with an EPDM or EPR rubbery phase dispersed through the polypropylene continuous phase, and (ii) any of LDPE, HDPE, metallocene catalyzed polyolefin, or linear low density polyethylene (LLDPE).

5 In another embodiment, the thermoplastic based elastomer is an alloy of (i) a thermoplastic vulcanizate comprising a polypropylene continuous phase with an EPDM EPR, NBR, NR or EVA rubbery phase dispersed through the polypropylene continuous phase, and (ii) any of LDPE, HDPE, metallocene catalyzed polyolefin, or linear low density polyethylene (LLDPE).

10 Suitable ion exchange resins include Rohm and Haas AMBERLITE™ IR120 and AMBERLITE™ IRA 402. Other suitable ion exchange resins include strongly basic anion and strongly basic cation resins with water content of less than 50 wt%, such as DIAION™ SA10A anion resin and DIAION™ SK1B cation resin manufactured by Mitsubishi Chemical Corporation. In another embodiment, the ion exchange resins are thermally stable and can be used to form high temperature ion exchange membranes which are configured to operate at temperatures > 80°C. An
15 example of a suitable high temperature anion exchange resin is DIAION™ TSA manufactured by Mitsubishi Chemical Corporation.

A heterogeneous ion exchange membrane can be manufactured using the binder polymers and ion exchange resins described above. The process includes resin drying, resin grinding, compounding of the ground resin and a binder polymer, and membrane sheeting.

20 IX resins have to be dried to lower their moisture content. Traditional ovens can be used to dry the resins. The heating temperatures are 60 to 120°C and the drying times are 0.5 to 24 hours.

A fluid bed dryer can be used continuously to dry the resins. The heating temperatures of a fluid bed dryer are 60 to 120°C.

The dried resins need to be ground before used in mixing (compounding) process. A conventional turbo mill can be used to grind IX resins. The particle sizes of the ground resins are controlled. In one embodiment, the particle sizes are from 20µm to 104µm.

The water contents of the ground resins may need to be controlled during the grinding process. In one embodiment, the final ground resin water content should not be more than 6 wt %. If the water content of the ground resin is too high, an extra drying treatment may be required.

The ion exchange resin is combined with the above-described binder polymer. In one embodiment, the weight ratio of the ion exchange resin to binder polymer is from 30/70 to 70/30. In another embodiment, the ratio is from 50/50 to 60/40. A twin screw extruder or a mixer(kneader) is used in the compounding process in the present invention. The compounding temperatures are from 80°C to 250°C, preferably from 120°C to 220°C. The compound, comprising an ion exchange resin and a binder polymer, is pelletized. If a kneader is used in the compounding process, a conventional type pelletizer is required to pelletize the compound to pellets. In one embodiment, the water content of the pellets is less than 1 wt%. If the water content of pellets is more than 1 wt%, the pellets need to be dried to decrease them to less than 1 wt% before they are employed in the extrusion sheeting process.

The compound of the ion exchange resin and the binder polymer fabricated from the previous process is used in the sheeting process to manufacture the membrane of the present invention. Extrusion molding, injection molding, compression-injection molding processing techniques can be employed in the present invention to manufacture ion exchange membranes.

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flattening and solidifying the extruded sheet and smoothing its surface. Thickness of the extruded and calendared material is measured by a nuclear gauge sensor 24. At this time, the first lip block 12 is at a first position. The sensor provides an electrical input signal corresponding to the thickness of the extruded and calendared material to a central processing unit (CPU) 22. The CPU 22 compares the input signal with a set point corresponding to a desired thickness of the extruded and calendared material. The CPU 22 then provides an output signal to one or more of the zones 16 of the second lip block 14 of the auto-die 10. In response to this output signal, the zones 16 are actuated and move relative to the first lip block 12 from a first position to a second position in the direction indicated by arrows 20, thereby adjusting the spacing between the zone or zones 16 and the first lip block 12 and achieving the desired spacing .

A second embodiment of the invention involves the injection molding of ion exchange membranes. This reduces the production cost and further ensures dimensional consistency and adequate phase dispersion. Injection molding eases the processing of beneficial binder materials that may not be ideally suited to extrusion with a filler material such as ion exchange resin particles.

Example

ENGAGE 8403™ was used as a binder polymer. The octene content in the ethylene-octene copolymer was 16wt%. ENGAGE 8403™ was characterized by the following physical properties: density was 0.913g/cm³, the melt index was 30dg/min, the surface hardness (Shore A) was 96, the ultimate tensile strength was 12.3Mpa, and the DSC melting peak temperature was 107°C.

A strongly acidic cation exchange resin, DIAION SK-1B manufactured by Mitsubishi Chemical Corporation, was used. The resin was dried by a fluid bed dryer at 105°C. The water

content of the dried resin was 3wt%. This dried resin was ground to the powdery resin. The particles with particle sizes of from 104 to 150 μ m were 0.8wt%, the particles with particle sizes from 45 to 104 μ m were 62wt%, and particles with particle sizes smaller than 45 μ m were 37.2wt%. This powdery resin was mixed with ENGAGE 8403TM by a twin screw extruder in a weight ratio of 60/40.

5 The extrusion temperature along the barrel varied from 165°C proximate the feed to 197°C at the die. The extrudate was pelletized to form 2mm diameter pellets. The water content of the pellets was measured to be 0.5wt%. The pellets were used directly in the extrusion sheeting process. A single screw extruder was used for the extrusion sheeting process. The extrusion temperature varied along the barrel from 130°C proximate the feed to 132°C at the die. The final membrane thickness was
10 500 \pm 10 μ m.

The final membrane was conditioned in 0.5N sodium chloride aqueous solution at 40°C for 1 days. The electrical resistance of the conditioned membrane was measured at an alternate current of 1,000Hz in a 0.5N sodium chloride aqueous solution. The resistance was 457 Ω .cm. The transport number of the conditioned membrane was also measured between 0.5N and 1.0N sodium chloride
15 aqueous solutions. The transport number was 0.872. The mechanical properties were tested by an Instron 4467 Universal Testing System. The tensile strength at yield was 2.5 MPa and the percent elongation was 138%.

It will be understood, of course, that modification can be made in the embodiments of the invention described herein without departing from the scope and purview of the invention as defined
20 by the appended claims.